



Experimental
Robotics

CS225A

Lecture 5

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Project Proposals
Experimental Robotics

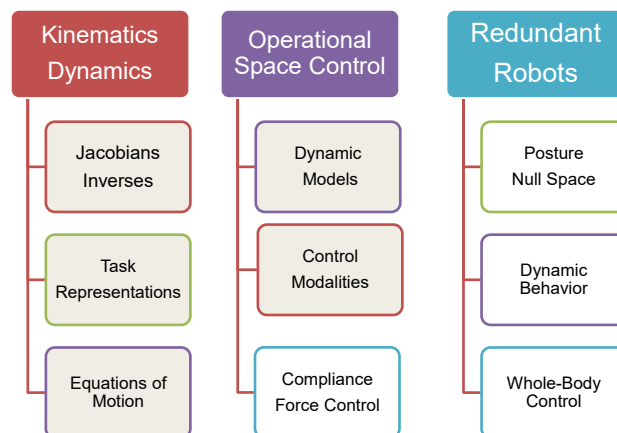
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Spring2021 Projects

Sports
Environment
Cooking
Groceries
Human Robot Interaction
Medical
Service

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Menu

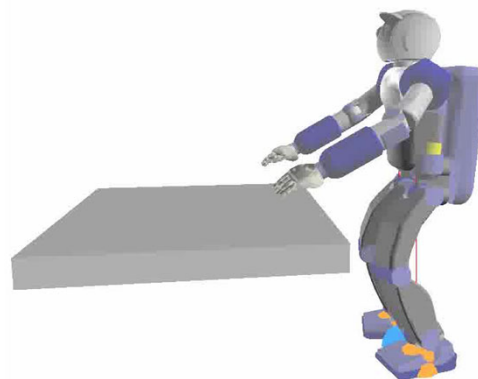
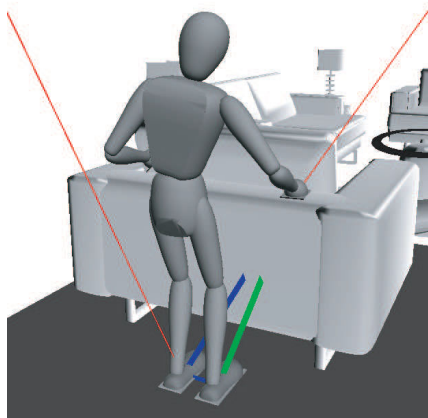


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Project Proposals Experimental Robotics

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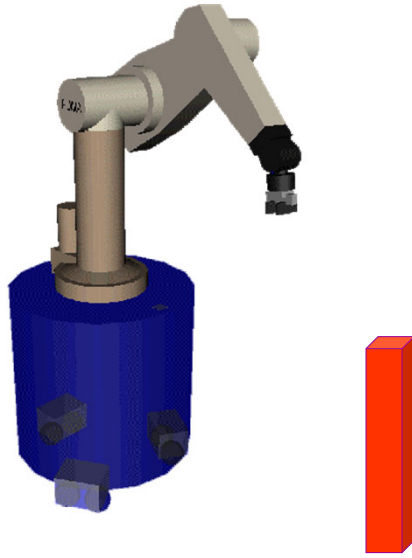
Operational Space Framework



.. motion in contact

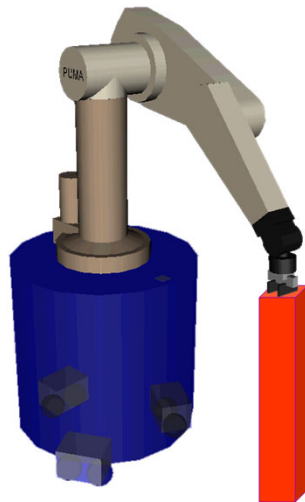
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Joint Space Control



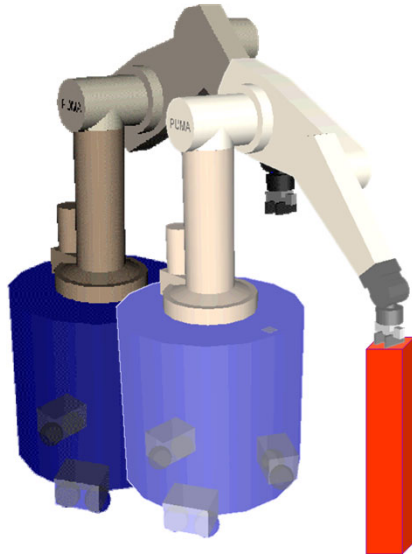
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Joint Space Control



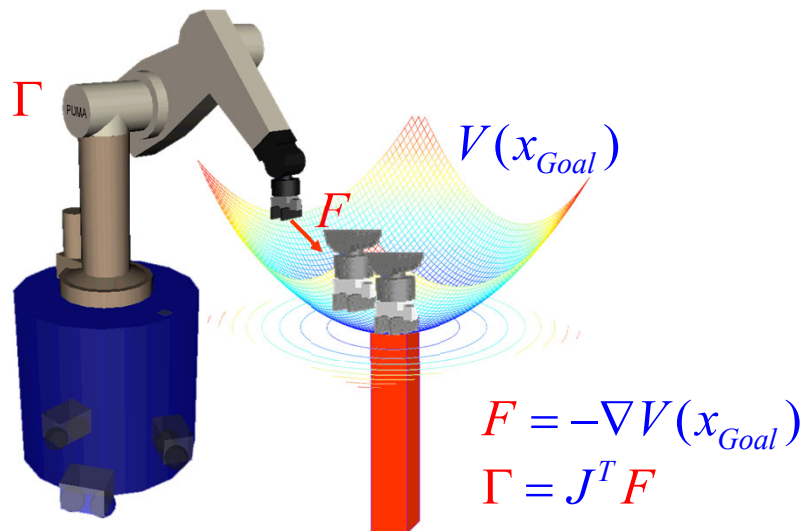
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Joint Space Control



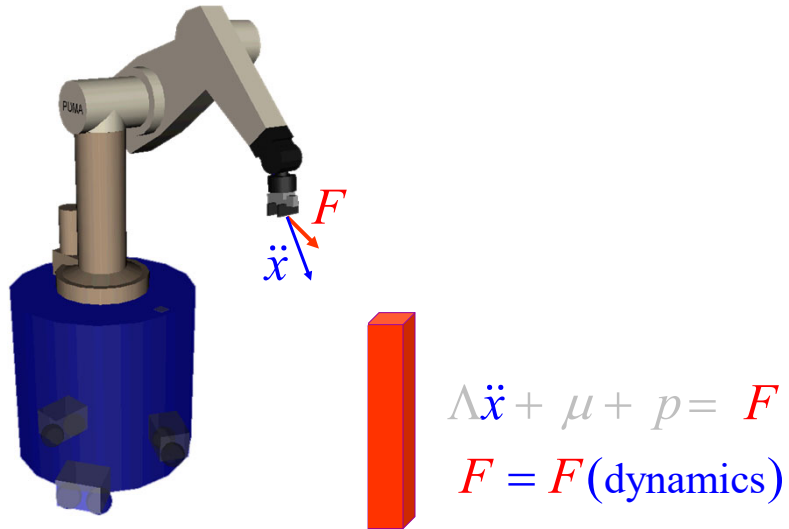
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Task-Oriented Control



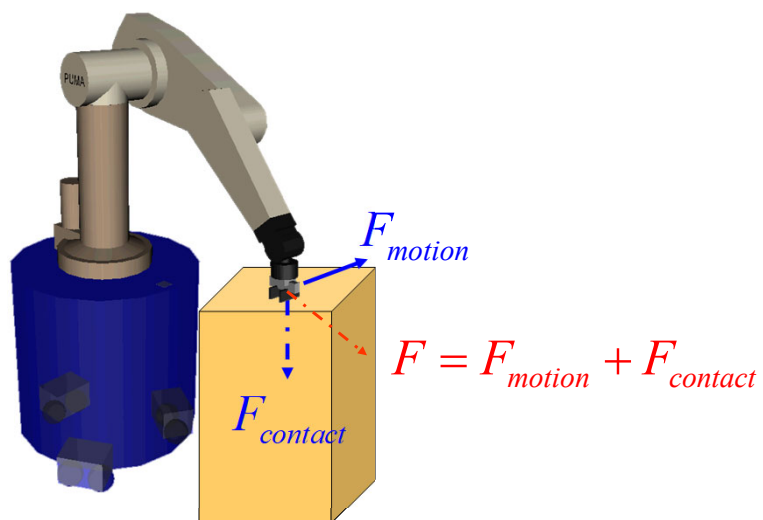
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Task-Oriented Control



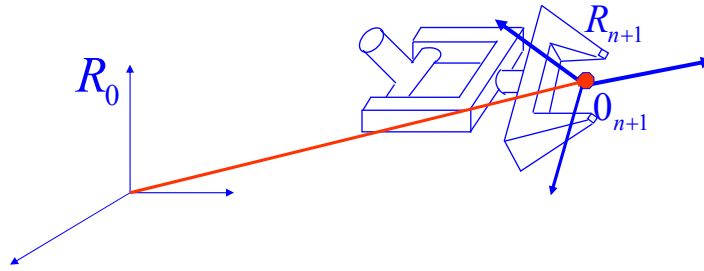
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Unified Motion & Force Control



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Effector Equations of Motion



Non-Redundant Manipulator ; $n = m_0$

$$x = (x_1 \ x_2 \ \dots \ x_{m_0})^T$$

$$q = (q_1 \ q_2 \ \dots \ q_n)^T$$

$$x = G(q)$$

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Lagrange Equations in Operational Space

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{x}} \right) - \frac{\partial L}{\partial x} = F$$

Lagrangian $\rightarrow L = T - V$

Kinetic Energy $\leftarrow T$

Potential Energy (Gravity) $\leftarrow V$

Since $V = V_{Gravity}(q)$

$$\Rightarrow \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial T}{\partial x} + \frac{\partial V_{Gravity}}{\partial x} = F$$

Inertial forces

Gravity vector

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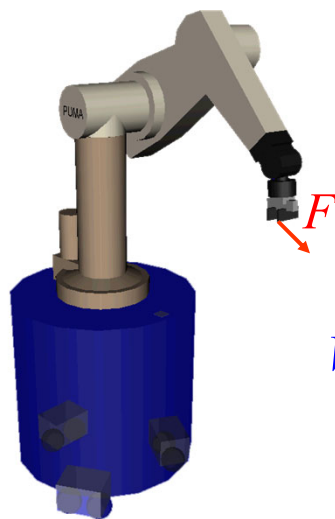
Operational Space Dynamics

$$\Lambda(x)\ddot{x} + \mu(x, \dot{x}) + p(x) = F$$

- x : End-Effector Position and Orientation
 $\Lambda(x)$: End-Effector Kinetic Energy Matrix
 $\mu(x, \dot{x})$: End-Effector Centrifugal and Coriolis forces
 $p(x)$: End-Effector Gravity forces
 F : End-Effector Generalized forces

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Operational Space Control



$$\Gamma = J^T(q)F$$

$$F = -\nabla V(x_{Goal})$$

$$V_{Goal} = \frac{1}{2} k_p (x - x_{Goal})^T (x - x_{Goal})$$

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Passive Systems

$$V_{Goal} = \frac{1}{2} k_p (x - x_{Goal})^T (x - x_{Goal})$$

$$\text{System } \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial (T - V_{Gravity})}{\partial x} = F$$

$$\Downarrow F = - \frac{\partial}{\partial X} (V_{Goal} - \hat{V}_{Gravity})$$

Conservative Forces

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial (T - V_{Goal})}{\partial x} = 0 \quad \boxed{\text{Stable}}$$

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Asymptotic Stability

$$\text{a system } \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{x}} \right) - \frac{\partial (T - V_{Goal})}{\partial x} = F_s$$

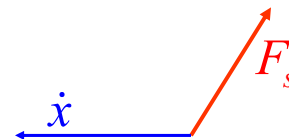
is asymptotically stable if

$$\boxed{F_s^T \dot{x} < 0 \quad ; \quad \text{for } \dot{x} \neq 0}$$

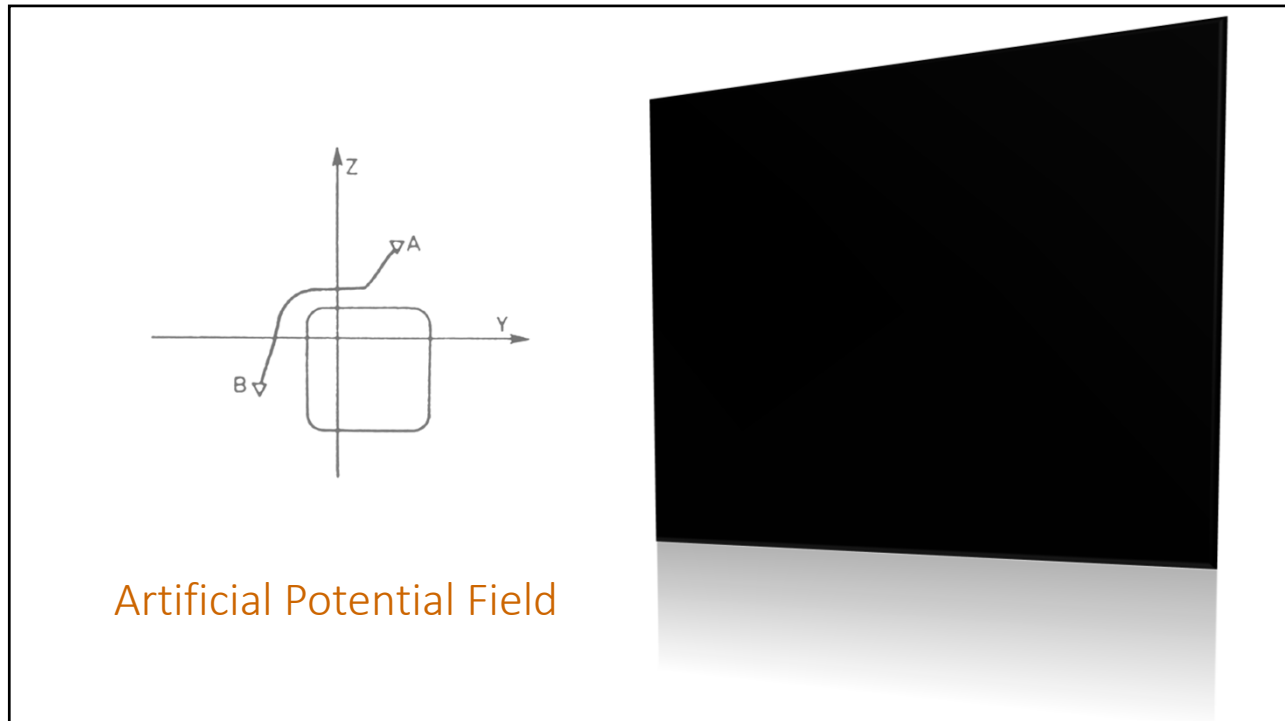
$$F_s = -k_v \dot{x} \rightarrow k_v > 0$$

Control

$$F = -k_p (x - x_{Goal}) - k_v \dot{x} + \hat{p} \quad \hat{p} \text{ Estimate of } p$$



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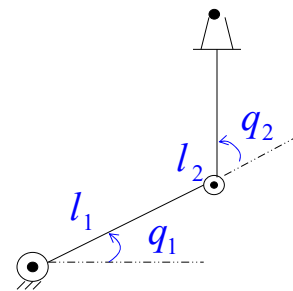


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Example: 2-d.o.f arm

$$\Lambda(x)\ddot{x} + \mu(x, \dot{x}) + p(x) = F$$

$$F = -k_p(x - x_g) - k_v \dot{x} + \hat{p}(x)$$



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$$(m_1^* c^2 + m_2) \ddot{x} + m_1^* \ddot{y} + \mu_1 = -k_p (x - x_g) - k_v \dot{x}$$

$$(m_1^* c^2 + m_2) \ddot{y} + m_1^* \ddot{x} + \mu_2 = -k_p (y - y_g) - k_v \dot{y}$$

Closed loop behavior

$$m_{11}(q) \ddot{x} + k_v \dot{x} + k_p (x - x_g) = -(m_1^* \ddot{y} + \mu_1)$$

$$m_{22}(q) \ddot{y} + k_v \dot{y} + k_p (y - y_g) = -(m_1^* \ddot{x} + \mu_2)$$

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Joint Space/Operational Space Relationships

$$T_x(x, \dot{x}) \equiv T_q(q, \dot{q})$$

$$\frac{1}{2} \dot{x}^T \Lambda(X) \dot{x} = \frac{1}{2} \dot{q}^T A(q) \dot{q}$$

Using $\dot{x} = J(q) \dot{q}$

$$\frac{1}{2} \dot{q}^T J^T \Lambda J \dot{q} = \frac{1}{2} \dot{q}^T A \dot{q}$$

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Joint Space/Operational Space Relationships

$$\Lambda(x) = J^{-T}(q) A(q) J^{-1}(q)$$

$$\mu(x, \dot{x}) = J^{-T}(q) b(q, \dot{q}) - \Lambda(q) h(q, \dot{q})$$

$$p(x) = J^{-T}(q) g(q)$$

where $h(q, \dot{q}) \doteq \dot{J}(q)\dot{q}$

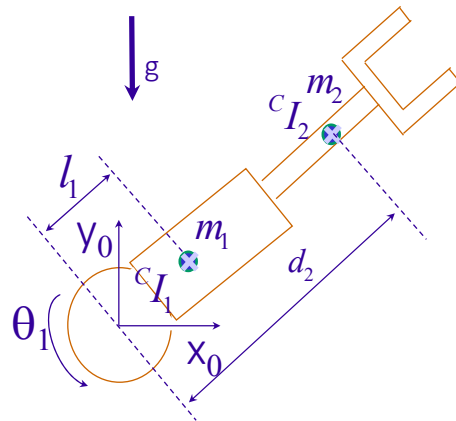
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Example

$$q_2 = d_2$$

$$x = \begin{bmatrix} d_2 c1 \\ d_2 s1 \end{bmatrix}$$

$${}^0 J = \begin{bmatrix} -d_2 s1 & c1 \\ d_2 c1 & s1 \end{bmatrix}$$



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$${}^0 J = \begin{bmatrix} -d_2 s_1 & c_1 \\ d_2 c_1 & s_1 \end{bmatrix}$$

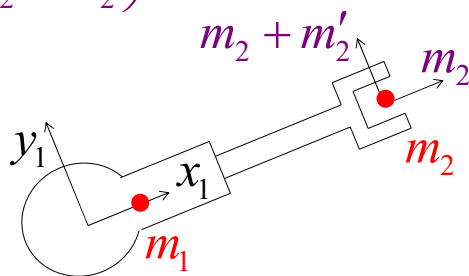
$${}^0 J = \begin{pmatrix} c_1 & -s_1 \\ s_1 & c_1 \end{pmatrix} \overbrace{\begin{pmatrix} 0 & 1 \\ d_2 & 0 \end{pmatrix}}{{}^1 J}$$

$${}^1 J^{-1} = \begin{pmatrix} 0 & 1/d_2 \\ 1 & 0 \end{pmatrix};$$

$${}^1 \Lambda = \begin{pmatrix} 0 & 1 \\ 1/d_2 & 0 \end{pmatrix} \begin{pmatrix} m_{11} & 0 \\ 0 & m_{22} \end{pmatrix} \begin{pmatrix} 0 & 1/d_2 \\ 1 & 0 \end{pmatrix}$$

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$${}^1 \Lambda = \begin{pmatrix} m_2 & 0 \\ 0 & m_2 + m'_2 \end{pmatrix}$$



$$m'_2 = \frac{I_{221} + I_{222} + m_2 l_1^2}{d_2^2}$$

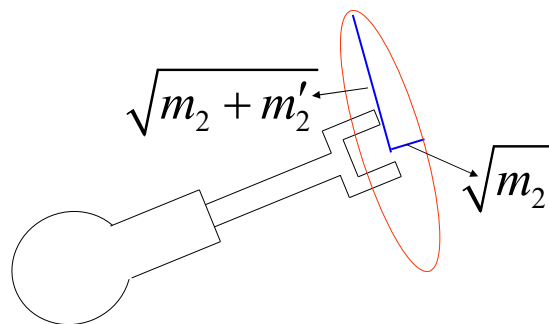
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$${}^0\Lambda = \begin{pmatrix} c1 & -s1 \\ s1 & c1 \end{pmatrix} \begin{pmatrix} m_2 & 0 \\ 0 & m_2^+ \end{pmatrix} \begin{pmatrix} c1 & s1 \\ -s1 & c1 \end{pmatrix}$$

$$m_2^+ = m_2 + m_2'$$

$${}^0\Lambda = \begin{pmatrix} m_2 + m_2' s1^2 & -m_2' s c1 \\ -m_2' s c1 & m_2 + m_2' c1^2 \end{pmatrix}$$

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$${}^0\Lambda = \begin{pmatrix} m_2 + m_2' s1^2 & -m_2' s c1 \\ -m_2' s c1 & m_2 + m_2' c1^2 \end{pmatrix}$$

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Nonlinear Dynamic Decoupling

Model

$$\Lambda(x)\ddot{x} + \mu(x, \dot{x}) + p(x) = F$$

Control Structure

$$F = \hat{\Lambda}(x)F^* + \hat{\mu}(x, \dot{x}) + \hat{p}(x)$$

Decoupled System

$$I \ddot{x} = F^*$$

$$\text{with } \Gamma = J^T F$$

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Dynamic Decoupling

$$\Lambda(x)\ddot{x} + \mu(x, \dot{x}) + p(x) = F$$

$$F = \hat{\Lambda}F^* + \hat{\mu}(x, \dot{x}) + \hat{p}(x)$$

$$I_{m_0} \ddot{X} = \underbrace{(\Lambda^{-1} \hat{\Lambda})}_{G(x)} F^* + \underbrace{\Lambda^{-1} (\mu - \hat{\mu})}_{\tilde{\mu}_{(x, \dot{x})}} + \underbrace{\Lambda^{-1} (P - \hat{P})}_{\tilde{P}(x)}$$

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Dynamic Decoupling: Closed Loop

$$I_{m_0} \ddot{x} = G(x)F^* + \varepsilon(x, \dot{x}) + d(t)$$

$$G(x) = \Lambda^{-1} \hat{\Lambda} \approx I + \varepsilon_\Lambda$$

$$\varepsilon(x, \dot{x}) = \Lambda^{-1} (\tilde{\mu} + \tilde{P})$$

$d(t)$: unmodeled disturbances

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Perfect Estimates

$$I_{m_0} \ddot{x} = F^*$$

F^* input of decoupled end-effector

Goal Position Control

$$F^* = -k_v \dot{x} - k_p (x - x_g)$$

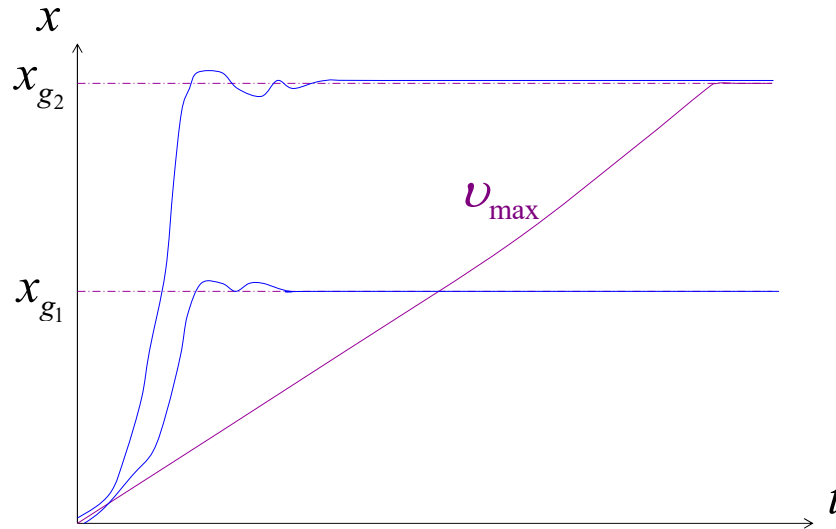
Closed Loop

$$I_{m_0} \ddot{x} + k_v \dot{x} + k_p x = k_p x_g$$

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Closed Loop

$$I_{m_0} \ddot{x} + k_v \dot{x} + k_p x = k_p x_g$$



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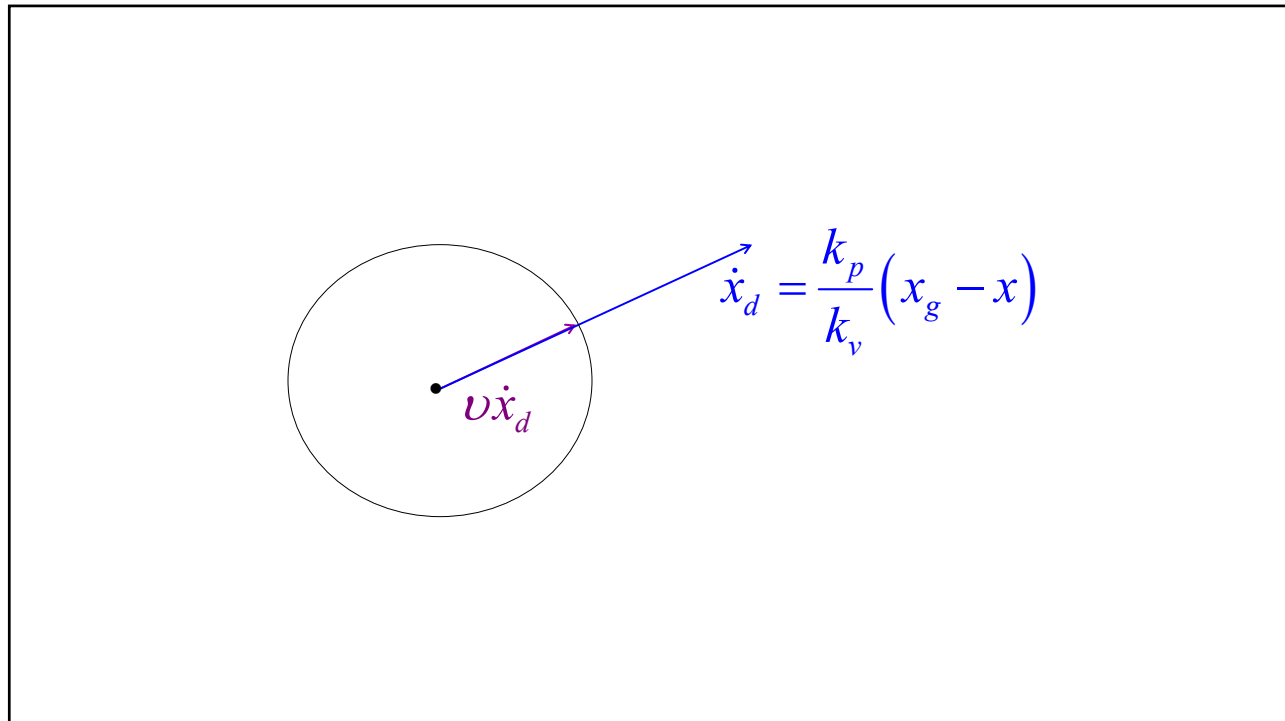
PD Control

$$F^* = -k_v \dot{x} - k_p (x - x_g)$$

Velocity-Like Control

$$F^* = -k_v \left(\dot{x} - \frac{k_p}{k_v} (x_g - x) \right)$$

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$$F^* = -k_v \left(\dot{x} - \underbrace{\frac{k_p}{k_v}(x_g - x)}_{\dot{x}_d} \right)$$

$$F^* = -k_v (\dot{x} - v\dot{x}_d)$$

with

$$v = \text{sat} \left(\frac{V_{\max}}{|\dot{x}_d|} \right)$$

$$\text{sat}(x) = \begin{cases} x & \text{if } |x| < 1 \\ \text{sign}(x) & \text{if } |x| > 1 \end{cases}$$

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Trajectory Tracking

Trajectory: $x_d, \dot{x}_d, \ddot{x}_d$

$$F^* = I_{m_0} \ddot{x}_d - k_v(\dot{x} - \dot{x}_d) - k_p(x - x_d)$$

$$(\ddot{x} - \ddot{x}_d) + k_v(\dot{x} - \dot{x}_d) + k_p(x - x_d)$$

or $\ddot{\varepsilon}_X + k_v \dot{\varepsilon}_X + k_p \varepsilon_X = 0$

with $\varepsilon_X = x - x_d$

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In joint space

$$\ddot{\varepsilon}_q + k_v \dot{\varepsilon}_q + k_p \varepsilon_q = 0$$

with $\varepsilon_q = q - q_d$

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